Analysis of Transformer Resonant Overvoltages Due to Switching Capacitance

[Koray Gürkan , Cengiz Polat Uzunoğlu , Serap Cekli , Mukden Uğur]

Abstract—**Power transformer transients, which are originated from non-linear operating characteristics, may cause failure of a power system. In this study, a special resonance phenomenon where overvoltages observed due to switching capacitances of the line is investigated. This situation is detected while high voltage side of the transformer is open circuit (no-load) and the low voltage side is connected to a transmission line through non-linear switch (or breaker). This special resonance is caused by the interaction of leakage inductance of the transformer windings and the switching capacitance. A test setup containing 220V/34.5kV transformer is employed for realization of simulation results obtained by SPICE analysis. In order to simulate switching capacitance, a capacitance of 5.54µF is connected to low voltage side. The recorded and simulated test results show good correspondence. Observed overvoltages are analysed by continuous wavelet transform (CWT) and fast Fourier transform (FFT) techniques. Also the energy distribution, which is generated by overvoltages, is investigated by instantaneous energy levels.**

Keywords—**switching capacity, power transformer, overvoltage, continuous wavelet transform, resonance**

I. Introduction

Resonance is a general term used for interactions between inductors and capacitors, which are employed to maintain the proper operation of power systems. Resonance phenomenon may cause unusual and disturbing overvoltages or currents [1].

Power transformers are the key components in power system connections and special measures should be taken into consideration to sustain overvoltage protection. Power transformer failures are not acceptable since the proper operation of a power system cannot be compromised [2]. Power transformer naturally contains leakage inductances originated from windings which are likely to cause resonance considering the capacitive effects of the line.

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During the operation of a power system the nonlinear inductance variations due to transformer core may lead to special kind of resonance which is known as ferroresonance [3]. There are some ongoing studies conducted on ferroresonance phenomenon [4-10].

In this study a 220V/34.5kV test transformer is employed to realize a special resonance condition due to switching capacitance of the line and the leakage inductance of the transformer windings. Transformer approximate equivalent circuit and transformer model are constructed. The leakage inductance and the leakage resistance of the transformer are calculated as 3mH and 1kΩ respectively.

The possible resonance capacity is obtained as 4µF by investigating nonlinear core model of test transformer and hysteresis curve. The resonance simulations are conducted properly by using SPICE and overvoltage waveforms observed. The real case scenario is fulfilled by using 5.54µF capacity as switching capacity which is slightly different from simulation. Due to approximations and tolerances of the simulation model real resonance is obtained by using reasonable switching capacitance.

During the tests overvoltage waveforms are recorded and analysed by using fast Fourier transform (FFT) [11-12] and continuous wavelet transform (CWT) [13-15]. The switching transients are displayed efficiently by CWT analysis and an early detection method of resonance initiation of power transformers proposed.

II. Test Set-Up

In this study a 220V/34.5kV test transformer is taken into consideration for resonance model. In order to obtain accurate simulation, corresponding transformer tests are carried out and SPICE parameters are obtained.

A. Estimation of Transformer SPICE Parameters

In this study resonance tests are simulated by SPICE model of the test transformer. To ensure the core-loss of transformer, an open circuit test procedure was conducted. After measurements core-loss is modelled with a 1 kΩ resistor. Initially to measure leakage inductance, secondary of the transformer is short circuited (Fig. 1). A capacitor of 470 nF is charged with an half-wave rectifier which rectifies main voltage. With using a SPDT switch, fully charged capacitor is suddenly connected to primary of transformer and transient oscillation at this point is recorded.
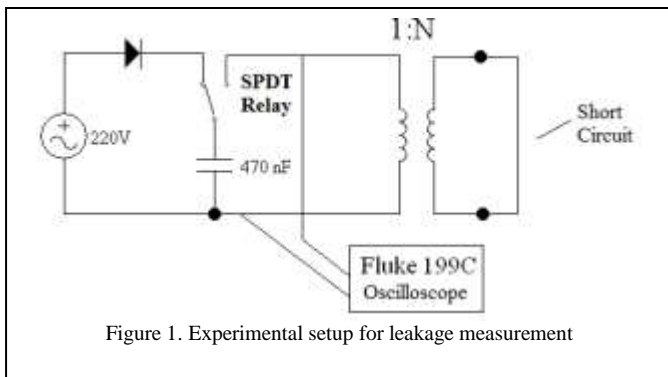
Figure 1. Experimental setup for leakage measurement

By calculating oscillation period, the leakage inductance is found as 3 mH. To predict non-linear B-H curve of transformer, input current and integral of voltage is displayed at dual trace oscilloscope with various input voltages (Fig. 2a). Here, Y channel corresponds integral of voltage and thus, flux linkage with 10x attenuation, and X channel corresponds to 1.6 times of current.
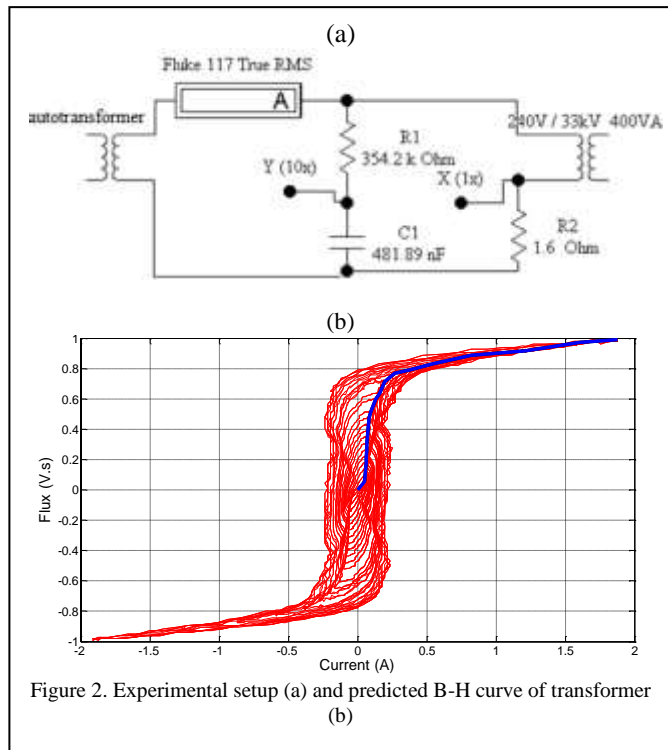

Figure 2. Experimental setup (a) and predicted B-H curve of transformer (b)

By using measured data, non-linear SPICE model of transformer is predicted by dividing B-H (Fig. 2b) curve into 15 coordinates which are obtained by different voltages supplied by autotransformer.

B. *Simulation Model*

The simulation model of the proposed switching scenario is given in Fig. 3. Leakage inductance of the transformer windings and transformer losses are represented by an inductance of 3mH and 1kΩ resistor, respectively.
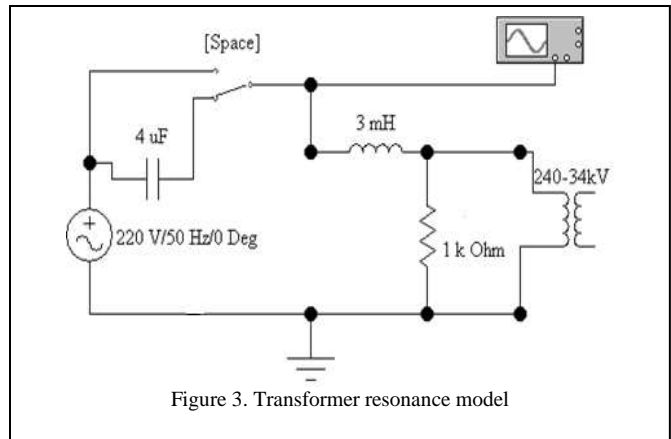

Figure 3. Transformer resonance model

In simulation, initially, transformer is directly operated under system voltage. By pressing the space bar on the physical keyboard, SPDT switch changes its state and transformer is now in series with capacitor. Switching characteristics of the Low Voltage (LV) line is simulated by 4 µF capacitor. A dry type 220V/34.5kV, 400VA, 50Hz test transformer, which is shown in Fig. 4 is employed to conduct real resonance tests.

Figure 4. Test transformer

An autotransformer is used for connecting primary side of the test transformer with power network. All signal waveforms are displayed and recorded by Fluke 199C scope meter. During the tests 470nF and 820nF capacitance combinations are used for obtaining 5.54µF capacity to realize resonance. All capacitors are designed to operate under 400V which is nominal voltage with tolerance for LV side. The test set-up is given in Fig. 5.
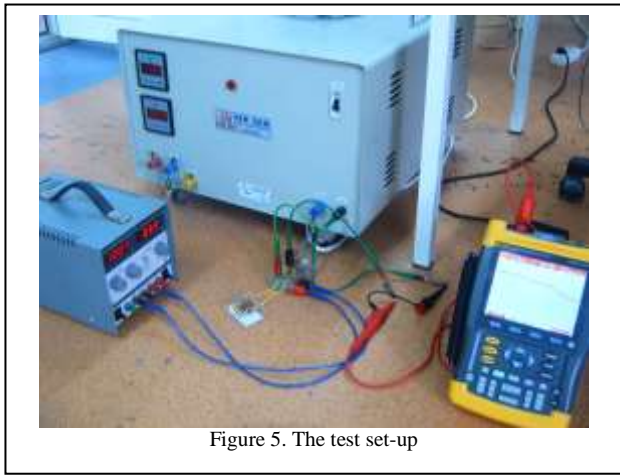
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Figure 5. The test set-up

III. Simulation Results

All simulations are conducted by using Electronic Workbench program. The resonance voltage waveform is obtained according to simulation model (Fig. 3) and given in Fig. 6. The switching initiation and transition to resonance mode can be easily tracked from figure.
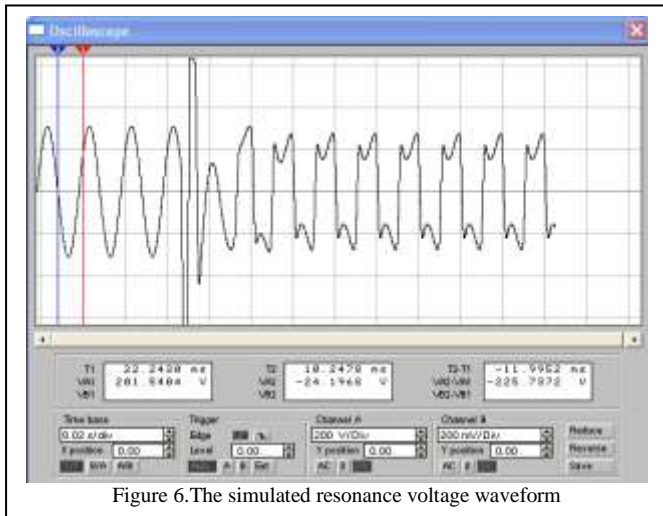

Figure 6.The simulated resonance voltage waveform

After initiation of resonance harmonics are observed on resonance voltage waveform. For this purpose FFT of voltage signal is analysed and frequency spectrum is given in Fig. 7.
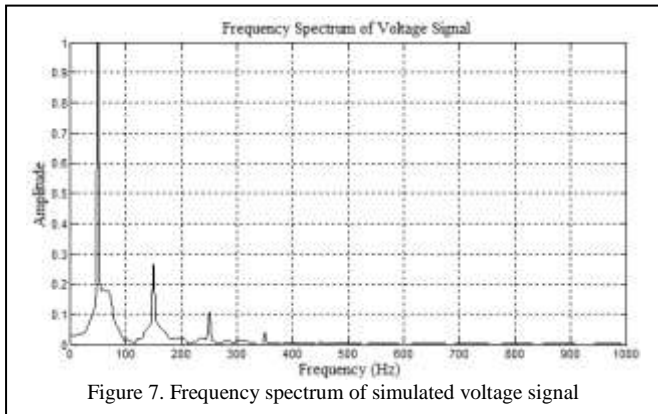

Figure 7. Frequency spectrum of simulated voltage signal

As seen from spectrum 3rd, 5th and 7th harmonics are dominant but higher harmonics are also observed.

IV. Experimental Results

The recorded real resonance voltage waveform of test transformer is given in Fig. 8. The real resonance signal depicts similar characteristics to the one obtained from simulation results. Switching transition and harmonics are observed on the signals. Also overvoltages up to 1.5 p.u. are detected during test period which are degradative for power system components.
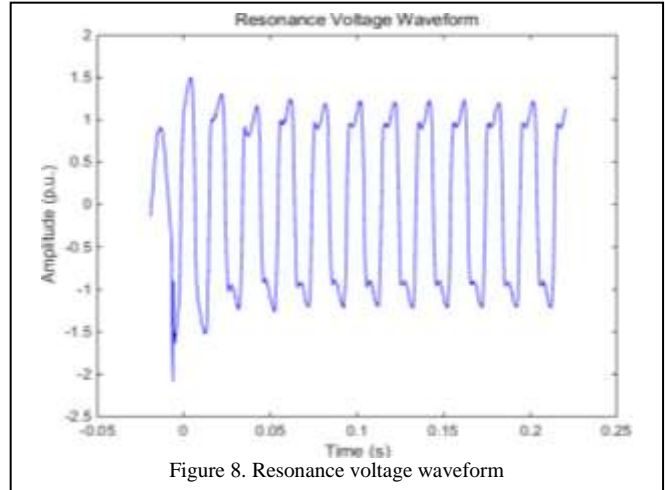

Figure 8. Resonance voltage waveform

In order to reach proper comparison, frequency spectrum of the resonance voltage is given in Fig. 9. Frequency spectrum of test results depicts similar results obtained from simulation results. In accordance with previous results 3rd, 5th and 7th harmonics are observed.
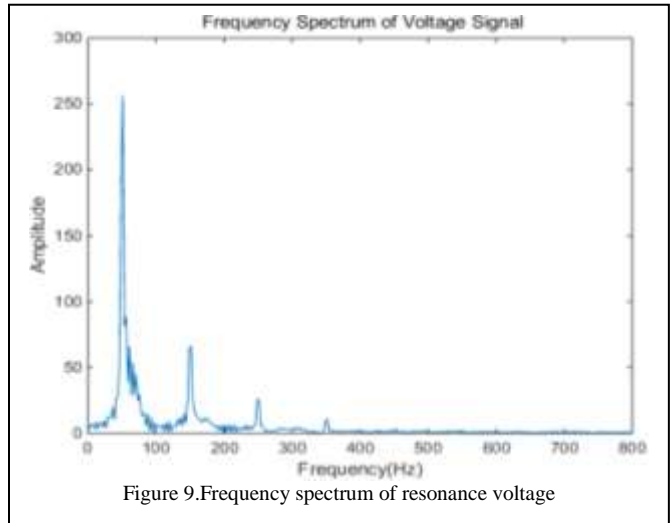

Figure 9.Frequency spectrum of resonance voltage

Beyond the FFT analysis, CWT analysis can concentrate on a limited time transition, which is displayed during the switching transients [13-14]. Peaks and oscillations are observed for limited time duration (few milliseconds). In order

to focus on quick transitions during switching, CWT of resonance voltage is given in Fig. 10.
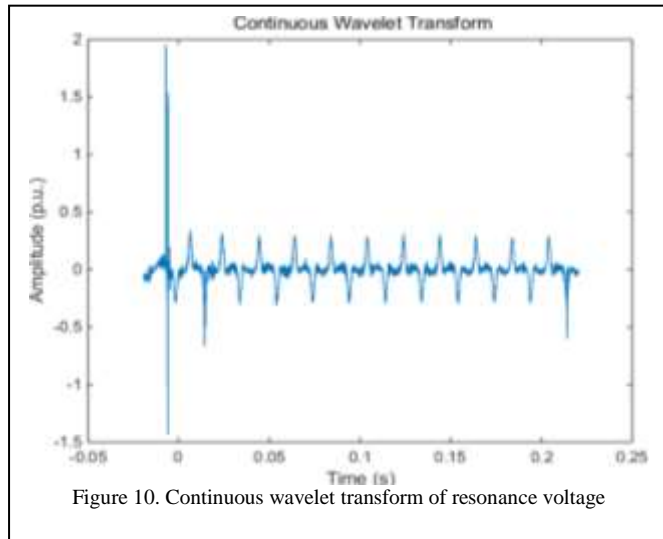

Figure 10. Continuous wavelet transform of resonance voltage

Some harmonic related transitions are displayed but most important of all the exact switching transition time can be detected with the corresponding amplitude value (2 p.u.). CWT signal transitions can reveal distinctive peak (resonance initiation) and point out system failure.

Since the instantaneous energy of non-stationary signals may represent distinctive characteristics, which has high oscillations and peaks, in this study resonance voltage signals are also analysed by energy levels. The instantaneous energy signal of resonance voltage is given in Fig. 11.
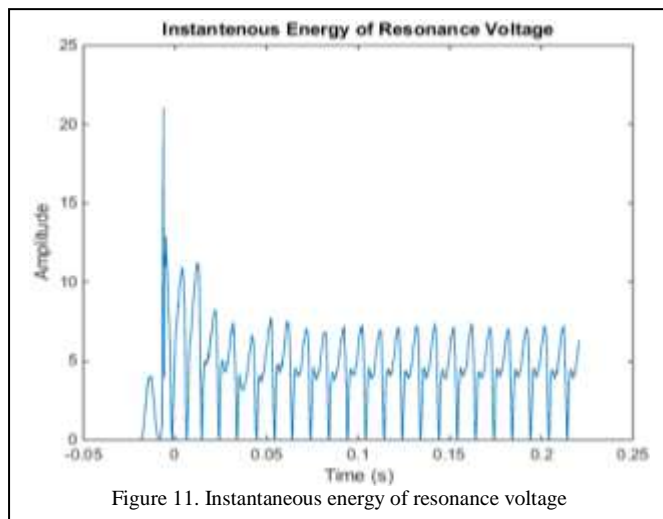

Figure 11. Instantaneous energy of resonance voltage

During the switching of power line instantaneous energy of voltage signal is increased approximately four times of the regular operation. After initiation signal has still two times of the regular operating state.

V. **Conclusions**

For the safe operation of a power system all components and corresponding signals should be observed constantly for failure. In this study a special resonance phenomenon occurred by unloaded transformer interaction with switching capacitance is investigated. During the resonance the unwanted transients such as overvoltages (up to 2 p.u.) and harmonics may cause failure of power system. Simulation results are supported with a real case scenario consisting test transformer. During the tests real capacitors are used to simulate switching capacitances. Test results depict very similar characteristic to the simulation results. FFT analysis showed that the resonance signal has higher harmonics which are capable of disruption of proper operation. Due to non-stationary signal characteristics of resonance voltages, CWT analysis is proposed for efficient detection of resonance. Also instantaneous energy level calculation method is proposed for investigation of resonance signals. During the initiation of resonance energy levels are increased significantly. Online detection of system voltage with proposed method may prevent system failure caused by unwanted resonance effect.

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